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MICROPROCESSOR CONTROL.

OF

QUARTER WATT LINEAR COOLER



FINAL REPORT

AUGUST 7, 1987

DECEMBER 5, 1986 TO JULY 31, 1987

Prepared under Contract Number DAABO7-87-C-F018 for Center for Night Vision and Electro-Optics

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MAGNAVOX GOVERNMENT AND INDUSTRIAL ELECTRONICS COMPANY ELECTRO-OPTICAL SYSTEMS, 46 INDUSTRIAL AVENUE MAHWAH, NJ 07430

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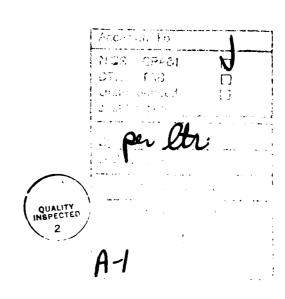
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A. Silver

Deputy Director of Engineering

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ABSTRACT

The work carried out in this study was performed by Magnavox Government & Industrial Electronics Company, Electro-Optical Systems, in accordance with the requirments of contract DAABO7-87-C-F018. The purpose of the program was to conduct studies of microcontroller/digital VLSI technologies for possible future use in cryogenic coolers.

A necessary condition that any electronic approach must satisfy in order to be considered for linear cooler electronics is the ability to work in the real time environment of 100 kHz or higher switching speeds. In the case of the existing analog design, this prerequisite has long been established to achieve practically sized line filters. Heretofore this speed was out of reach of microprocessor based, controllers since the state-of-the-art was somewhere in the neighborhood of 8 to 10 kHz. However, a new device on the market has provided the necessary interface hardware to bridge this gap. This advancement combined with the advances of microcontrollers in terms of cost, size, and performance suggested that an investigation of the microcontroller/digital approach for the Magnavox quarter watt cooler electronics be performed.

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1.0 INTRODUCTION

The work carried out in this study was performed by Magnavox Government & Industrial Electronics Company, Electro-Optical Systems, in accordance with the requirments of contract DAABO7-87-C-F018. The purpose of the program was to conduct studies of microcontroller/digital VLSI technologies for possible future use in Magnavox cryogenic coolers.

1.1 MOTIVATION FOR MICROPROCESSOR/DIGITAL CONTROL

The present technology used for Magnavox cooler linear motor control is based on an analog circuit design. The diagram shown in Figure 1 is representative of the approach to meet a requirement for closed-loop cold station temperature control. Although this analog design functions well, there are compelling reasons to look in the direction of microcontroller/digital electronics, Figure 2, for future designs.

The first and most important reason is potential cost savings. The analog approach requires hand assembled control hybrids with expensive laser trimming. This is in contrast to the microcontroller approach that utilizes low cost, mass produced IC's.

A second potential benefit from a microcontroller approach is accuracy. A performance advantage is achieved in maintaining accurate temperature control of the detector cold station. As the tolerance on temperature is tightened the cost for accurate trimming of the analog design increases exponentially. In the case of the microcontroller, accuracies to $\pm 1\,^{\circ}\text{K}$ are easily attainable. Additionally, long term thermal drift, and component variability, are not a concern.

There are advantages in flexibility. Such things as customer requirements for the temperature set point or specialized modes of operation to conserve power can be satisfied by simple changes in software. New drive wave forms, easily generated in software, could have a favorable impact on efficiency and/or reduction of mechanical vibration.

1.2 SWITCHING FREQUENCY

With these advantages, summarized in Table 1, the natural question is why weren't microcontroller electronics used sooner? The answer is that the volume constraints on the cooler electronics requires that the swtiching frequency of the power amplifier be above 100 kHz. As the frequency is reduced from this level the input EMI filter components tend to grow. Since they just fit now, any growth would mean a deterioration in the performance of the filter.

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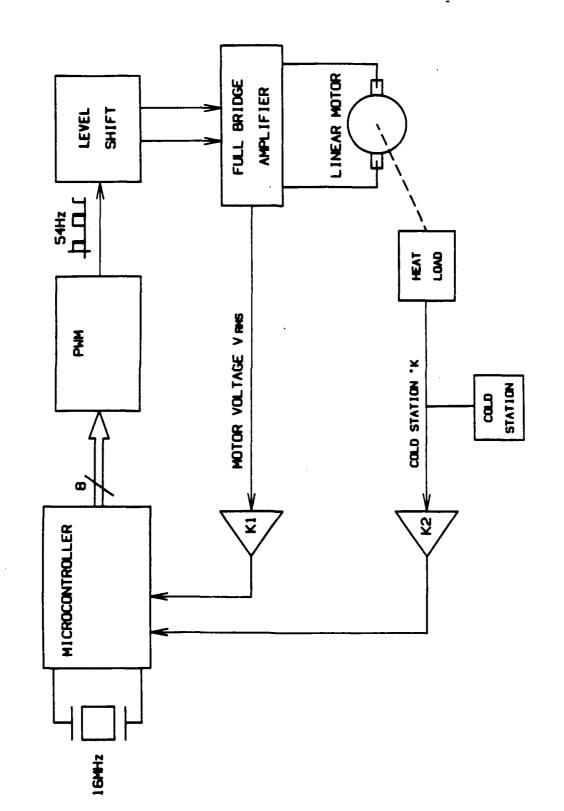


FIGURE 2

Table 1. Relative Comparison of Analog Versus Digital Design

	Analog Control	Digital Control
Parts Count	High	Low
Flexibility	Low	High
High Volume Cost	High	Low
Low Volume Cost	Low	High
Reliability	Good	Better
Accuracy	High	High

Specifically, the volume available in the cooler for the electronics is 0.7 cubic inches. The analog package as it is currently configured just fits into this volume - no margin for expansion. Of that volume approximately 20% is occupied by the input EMI filters. These components are designed for the 100 kHz switching frequency. If we were to lower the frequency by a decade, the volume occupied by the filter chokes would increase by approximately 50% to maintain the same impedance level. The filter capacitors would have to be increased by 3 to 4 times depending on ripple considerations. For these reasons, switching frequencies in the range of 10 kHz are out of the question.

As mentioned previously, until recently 100 kHz real time control was out of reach of microcontroller technology. This would require algorithmic execution speeds in the order of 10 microseconds which is out of reach for present day microcontrollers. However, a new interface PWM chip overcomes this and is a focus of attention for this study.

2.0 DESCRIPTION OF HARDWARE

2.1 COMPUTER

The design shown in Figure 2 represents a production concept for the microcontroller/digital electronics. Note that this is closed loop on both motor voltage and cold station temperature. To achieve this, the basic functions of the microcontroller are:

- 1. Get the appropriate PWM level from the data stored in memory.
- 2. Multiply that number (thereby changing the gain) to adjust for variation of motor voltage from command set point.
- 3. Multiply a second time (again modifying the gain) to adjust for variations in thermal loading.
- 4. Write to the digital PWM chip the appropriate code in accordance with the above calculation.

A typical microcontroller, as shown in Figure 3 is a single chip microcomputer. It is compatible with all system timing, internal logic, ROM, RAM and I/O. Although it is not obvious in Figure 2, the microcontroller has on board the required A/D converters for closed loop control.

For the purpose of a demonstration it was convenient to use a "single board computer" (SBC) to simulate functions of a microcontroller. The arrangement shown in Figure 4, used an Ampro SBC, with the Intel 80186 microprocessor, and was programmed by an Applied Microsystem, ES 1800 Satellite Emulator. This provided easy manipulation of the code through PL/M on the PC.

2.2 DIGITAL PULSE WIDTH MODULATOR (DPWM) - IXDP610

The ability to reach switching frequencies greater than 100 kHz is achieved by the IXDP610 Digital Pulse Width Modulator (DPWM) chip. This chip is a major breakthrough in high frequency motor control applications. Without it switching would be limited to approximately 8 kHz. As discussed previously, this would eliminate consideration of the microcontroller approach.

A block diagram of the IXDP610 (DPWM) is shown in Figure 5. The programmable, CMOS, LSI device receives digital pulse width data (8 bits) from the microcontroller and generates a TTL pulse width modulated signal. The DPWM is designed for direct control by the microcontroller. Current limiting on a cycle by cycle basis can be asserted through "Output Disable Logic" (ODIS).

2.3 TIMING DIAGRAM

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The timing diagram of Figure 6 shows the digital aspects of this topology. Figure 2, shows that the master clock is crystal controlled and set at 16 MHz. This clock signal together with the appropriate input to the programmable digital PWM controller, sets the switching frequency as follows:

PWM base period = Clock Period x 128

8 Microsecond (125 kHz) = 63 nanoseconds (16 MHz) x 128
The rate at which the CPU strobes through the look up table is
controlled by a programable counter which is fed by an external 125 kHz signal.
The counter is set to count 25, 8 μs counts (8 μs x 25 = 200 μs). Upon
decrementing to a 0 count, an interrupt is pulled. At this time the current
value is taken out of the look up table, outputted to a port and the table
pointer incremented. This data is outputted to the IXDP610 latch. With the
"Chip Select" low, the data is written to the pulse width latch. Under the
steady state mode of operation, the pulse width of the power amplifier is fixed
for the next 200 μs, after which another CS pulse will allow an update.

2.4 LEVEL SHIFT AND POWER AMPLIFIER

With a TTL pulse width modulation signal from the DPWM chip, the next requirement is to amplify the signal and drive the motor. This part of the

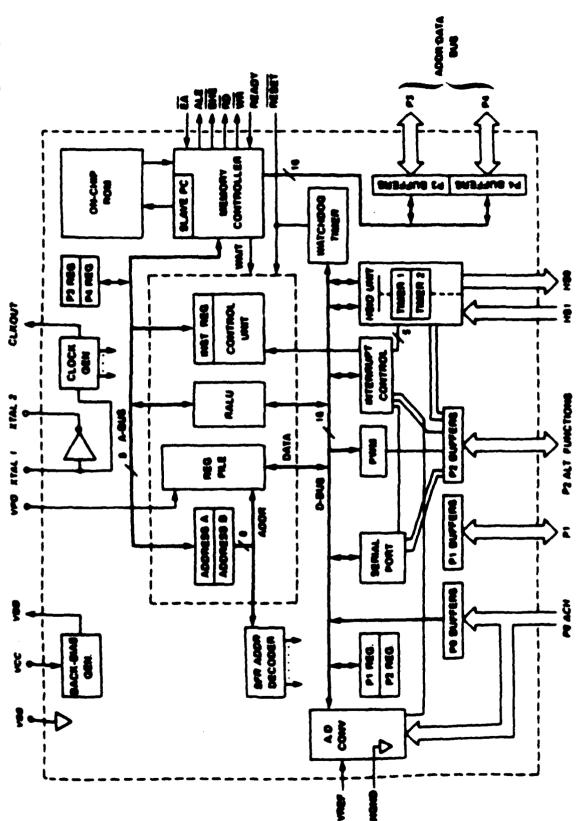
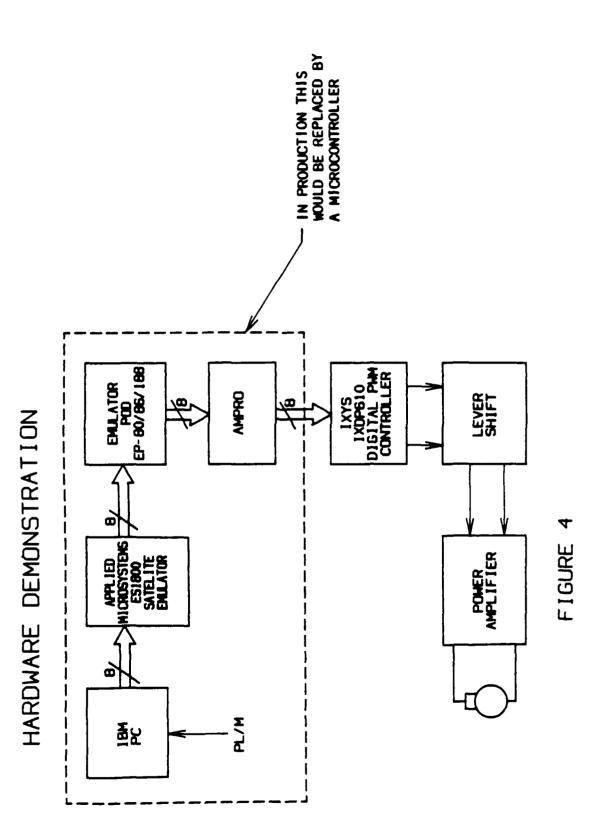


FIGURE 3



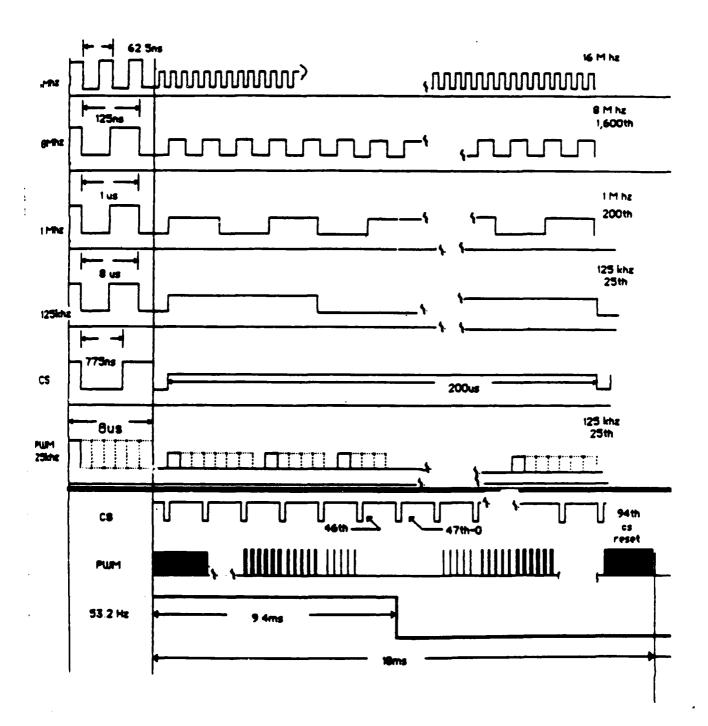
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FIGURE 5.

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FIGURE 6. Timing Diagram

design is common to both the analog and the digital approach - no significant difference.

3.0 DESCRIPTION OF SOFTWARE

Algorithms were developed to implement open loop control of the cooler motor. A fixed input line voltage (24 Vdc) was assumed. A flowchart of this software is shown in Figure 7, with code, as developed using PL/M, listed in Appendix I.

Lookup Table (Table 2)

For the demonstration, the function of the computer was to update the DPWM chip with an 8 bit digital input. Basically, by means of the lookup table it is generating a digital sine wave command signal. The theory behind the development of the lookup table is very basic.

Analog Sine Wave: $V(t) = Vm \times sine (2xPIxf) \times k \times d$

Vm = peak motor voltage (14 volts)

f = motor frequency (54 Hz)

v(t) = instantaneous motor voltage

k = sample point

d = sampling interval

The voltage v(t) is the sample value of the required cooler motor voltage at time $k \times d$. The sampling interval for demonstration was approximately 200 microseconds. Therefore the sine wave is approximated by steps that change every 200 microseconds, or 94 steps.

To generate the table therefore only the first half of the sine wave need be sampled or approximately 9.25 milliseconds for a 54 Hz sine wave. The values for a 14 volt peak or 9.89 Vrms sine wave are listed in column 2 of Table 2. The relationship between these voltage levels and the Pulse Width Modulator or Duty Cycle signal is as follows:

 $v(t) = (Ton/T) \times Vin = PWM \times Vin$

PWM = pulse width modulation level (range 0 - 1.0)

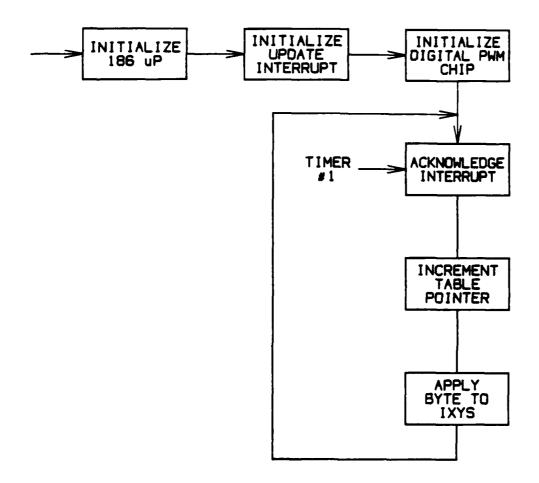
T = switching period

Ton = on time of power switches

Vin = line voltage

Since we were operating open loop, the line voltage (Vin) was set to be constant at 24 Vdc. With this level established, the corresponding PWM levels are shown in column 3 of Table 2. These levels are then converted to the nearest hexidecimal number as listed in column 4 of Table 2.

SOFTWARE FLOWCHART



Section to second the second s

FIGURE 7

POINT	VOLTS (Vt)	DUTY CYCLE (PWM)	HEX NO.
POINT 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37	0 .9346235 1.865077 2.787209 3.696905 4.590107 5.462829 6.311178 7.131367 7.919739 8.672775 9.387114 10.05957 10.68715 11.26704 11.79666 12.27365 12.69588 13.06146 13.36876 13.80333 13.92864 13.99181 13.99256 13.99181 13.99256 13.99181 13.99256 13.93087 13.62159 13.37537 13.06947 12.70526 12.28436 11.80866 11.28026 10.70154 10.07507 9.403646 8.690269		000h 00Ah 014h 01Eh 028h 031h 044h 055h 065h 065h 077h 088h 087h 092h 093h 094h 095h 095h 095h 087h 095h 095h 087h 095h 095h 095h 095h 086h 087h 095h 095h 095h 095h 095h 095h 095h
38 39 40 41 42 43 44	7.938118 7.150549 6.331073 5.483353 4.611168 3.718409 2.80906 1.887177	.3307349 .2979396 .2637947 .228473 .192132 .1549337 .1170441 7.863237E-02 3.986962E-02	044h 03Bh 031h 028h 01Eh 014h 00Ah 000h
46	.9568709	J. 700702E-02	÷ • ·

Table 2. Look Up Table

Note that on page 7 of the code listed in Appendix I, the lookup table is listed in accordance with Table 2. We emphasize again that this table is correct for 24 Vdc line voltage only and that in a final design will have to be scaled to accommodate a changing input line.

In addition to the lookup table, for the demonstration to be successfully implemented, algorithms were developed for the following functions:

- 1. Initialize Processor
- 2. Initialize Counter #1 this counter controls the lookup table pointer counts pulses at a 125 kHz clock and increments evey 25 counts
- Initialize PWM chip (IXDP610) i.e., deadtime set, lock bit off, 8 bit resolution.

4.0 SURVEY OF MICROCONTROLLERS

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The heart of the microcontroller/digital approach to the motor driver electronics is the microcontroller. From the conception of the microprocessor in 1974 there have been many advancements in the VLSI technology of microprocessors. Improvements have steadily been made in performance such as processor speed, bus size and power consumption. However, probably most startling of all was the advancements in the ability of the IC manufacturers to pack more functions into a given area of substrate. It was the improvements made in the small size of the substrate that has made the evolution of the microcontroller possible.

A microcontroller differs from a microprocessor in that it is a self contained computer. Unlike a microprocesor it needs no support chips, and in fact, packs more function in the form of A/D converter, UART serial communication, interrupt controls and I/O. For these reasons Magnavox believes that a microcontroller is a natural progression for the next generation cooler electronics.

The major manufacturers of microcontrollers are: Intel, Motorola, National and Texas Instruments. Table 3, is a matrix that compares the existing microcontrollers and provide some of the primary features that relate to the cooler application. It should be pointed out that these features are as they exist at the time of this writing and because of the rapidly changing technology they would have to be reexamined again at the time of a design effort.

	IATEL	MOTOROLA	NATIONAL	TEXAS INSTRUMENTS
Family	9608~SDH	м68нс11	HPC16084	7000 Series
Φ/0	10 Bit	4 Channel, 8 Bit	Not Yet	No
Bus	16 Bit	16 Bit	16 BIC	8 Bit
PWM Output	Yes	No	Yes	No
Watchdog Timer	Yes	Хев	Yes	No
Timer	7	5	8	3
No. I/O Ports	\$	5	5	-
Interrupt Sources	20	91	8	ť
Power Consumption	100 mW	3 Modes Run - 50 mW Wait - 3 mW Stop - 1 mW	100 MM	100 mW
RAM	256 K	256 K	256 K	256 К
КОМ	8 K	8 K	8 K	7 Y
Price (Commercial)	91\$	91\$	Not Available	Not Available
MIL	Avail. In MIL	Will Be Avail.	Will Be Avail.	No
Software Develop- ment Status	Available	Available HDS-300	Available (Mole)	Available

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Table 3. MICROCONTROLLER SURVEY

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5.0 SELECTION OF SWITCHING FREQUENCY

5.1 VOLUME CONSTRAINT

The reason for the popularity of a PWM SWITCHMODE power driver is that this approach is very efficient. The theory behind this is that in the ideal, there are only two states for the switching devices — "on" and "off". In the "on" state we assume no voltage drop across the device and in the "off" state, no current flow. Therefore, in the ideal case no power is dissipated in the power amplifier. However, looking at the real device, there is a finite voltage drop when the device is "on" and a finite current when the device is "off". Furthermore there are switching losses when the devices change state. These losses increase with frequency.

This implies that from an efficiency point of view, it is best to keep the power amplifier switching frequency as low as possible. However, for the cooler electronics an overriding consideration is volume. For that reason, and as discussed earlier, the switching frequency must be above 100 kHz. Specifically, the size of the EMI components are frequency dependent and at frequencies much below 100 kHz, they do not fit.

5.2 DIGITAL HARDWARE CONSTRAINT

With the approach described we have hardware that can potentially switch up to 200 kHz. However, due to the requirements of the counters we have a practical constraint to choose frequencies that are divided by two, submultiples of the 16 MHz clock. This breaks down to frequency choices of 125 kHz, 62.5 kHz and 31.25 kHz. A frequency of 125 kHz was selected in accordance with the 100 kHz limitation described above.

5.3 THE SELECTION

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At the present time 125 kHz is the best estimate of the optimum switching frequency. In future design efforts we would not expect any new inputs that would cause significant deviation from this frequency choice. However, the number of switching levels that go into the sine wave may vary since this number may influence the vibration profile of the cooler.

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6.0 SUMMARY

The work carried out in this study was performed by Magnavox Government & Industrial Electronics Company, Electro-Optical Systems, in accordance with the requirments of contract DAAB07-87-C-F018. The purpose of the program was to conduct studies of microcontroller/digital VLSI technologies for possible future use in Magnavox cryogenic coolers. In pursuit of this

objective, the following specific tasks were required of the study:

Task No. 1: Study of Single Chip Microcomputers

Task No. 2: Determine Optimum Pulse Width Modulation Frequency

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Task No. 3: Develop Algorithms

Although the scope of this study was initially conceived to be a white paper report/study only, Magnavox has taken the initiative to implement the basic concepts with a hardware demonstration. That is, a microcontroller was simulated using an Intel 80186 microprocessor and configured to drive an operating cooler. This clearly substantiates the microcontroller/digital approach and is planned as a demonstration for cognizant CNVEO personnel.

7.0 RECOMMENDATIONS FOR FURTHER STUDY

Based on the positive findings of this research effort it is recommended that additional funding be provided to implement a high switching frequency microprocessor/digital design program to further refine the cooler electronics. Specific tasks recommended for investigation include:

- Investigation of nonsinusoidal motor voltage drive waveforms. This would be implemented by appropriate changes in the software. The potential benefits from this investigation would be lower vibration levels and increased operating efficiency of the cooler.
- 2. Investigate "SMART" cooler electronics. Self calibration, self test and diagnostics are a few of the possibilities to be explored.
- 3. Develop optimum stepped sinusoidal waveform. This will require careful analysis before establishing a firm number for the design.
- 4. Explore use of feedback signals representing the working gas temperature or pressure. Determine the effects of these signals on cooler performance, i.e., stability of temperature set point, efficiency and vibration.

APPENDIX I

DEMONSTRATION SOFTWARE

IBM PC-DOS PL/M-86 V2.3 COMPILATION OF MODULE INTIB6

DOLLARS

ELECTION OF

PRODUCED RECEIPED PROCESSES

```
OBJECT MODULE PLACED IN INTIBA.OBJ
COMPILER INVOKED BY: PLMG6 INTI86.PLM DEBUG KREF CODE MODI86
  1
            INT186:
              nn:
  2 1
              DECLARE FLAG BYTE EXTERNAL;
                STARTING OF INITIALIZTION OF APX186, AND 2681 DUART'S
                UMCS is initialized in ase program STRTSE6 at OFFFOR
                3 1
                Declare
                                                /* Chip select register locations*/
                  LHCS REG
                           literally 'OFFA2h',
                  PACS REG
                            literally 'OFFA4h',
                  MPCS REG
                            literally 'OFFABh',
                  MLOC REG
                           literally 'OFFA6h';
                Declare
    ı
                             /# Timer control registers locations#/
                  t2mode_reg_literally 'OFF66h', /* Timer 2 mode control word */
                  t2maxa_req literally 'OFF62h', /* Timer 2 max counter A
                  t2count_reg literally 'OFF60h', /# Timer 2 counter register #/
                  tleode req literally 'OFF5Eh',
                  tleaxB_reg_literally 'OFF5Ch',
                  timaxA reg literally 'OFF5Ah',
                  ticount_reg literally 'OFF58h'
                  tOmode_reg_literally 'OFF56h',
                  tomaxB_reg literally 'OFF54h',
                  tomaxA_reg literally 'OFF52h',
                  tocount_reg literally 'OFF50h',
                  timer_int literally 'OFF32h';
  5 1
                Declare
                                     /* DMA control registers locations */
                  dmaO_cntrl_reg_literally 'OFFEAh', /*DMA channel O control word */
                  dma0_count_reg_literally 'OFFCSh', /#OMA channel 0 transfer counter#/
                  dmaG_dest_H_reg_literally 'OFFCah', /+DMA channel O destination high ptr+/
                  dma0_dest_L_reg literally 'OFFC4h', /+OMA channel O destination low ptr +/
                  dme0 src H_req literally 'OFFC2h', /+DMA channel O source high pointer +/
                  dma0_src_L_reg literally 'OFFCOh', /+OMA channel O source low printer +/
                  dmai_cntrl_reg literally 'OFFDAh',
                  deal_count_reg literally 'OFFD8h',
                  deal_dest_H_reg_literally 'OFFD6h',
                  dual_dest_L_reg_literally 'OFFD4h'.
                  dual_src_H_reg_literally 'OFFD2h',
                  dmal_src_L_reg literally 'OFFDOh';
    1
                Declare
                  t0eade
                                literally 'OCOO3h',
                                literally 'OE005h',
                  tleode
                                literally 'OCOOIh', /* enj/inh;count true */
                  t2mode
                                literally '014F7h';
                  claude
```

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```
7 1
            Declare
             MCS_SIZE literally '008Fh', /*acs size is 00.programed only to set */
                       /* peripheral map to 1/0 space & Al-A2 not*/
                       /# latched.#/
             PACS LOC literally '0130h'; /# peripheral chip setect base addr = 1000h#/
                                 /# one wait states for pacs0-3; 3-wait for 4-64/
                     /# external ready ignored for all pacs's
             Init186: PROCEDURE PUBLIC:
              Outword(MPCS RE6) =MCS_S[ZE; /*init midrange block size */
              Outword(PACS REG) =PACS LOC: /#init peripheral chip select #/
10
   5
             Outword(t2mode_REG) =t2mode; /+timer 2 set for RAM refresh +/
  2
11
              Outword(t2maxA_RE6) =320;
                                     /#timer 2 set for 16 u/s rat #/
15 5
13 2
              Outword(t2count_RES) =00h;
             /# Counter-1 is set up to count 25 125khz Pulses then start a
                interrupt for a count of 200us #/
   2
                 Outword(timer_int) = 0000;
14
15
              Outword(tlmode_REG) =tlmode;
              Outword(tlmaxA_REG) =019h;
                                      /# 25 counts #/
16
  5
              Outword(tleaxB REG) =00000h;
17 2
              Outword(ticount_REG) =00h;
19 5
             /# DMA is programmed for a memory-to-1/0 transfer, with writes
               to nonexistant I/O space. The DMA is programmed to continuously
               run through the entire segabyte of sesory at word transfers #/
19
   2
              Dutword(dmai_dest_H_reg) =OFFh;
20
              Outword(deal_dest_L_reg) =OFFh;
15
              Outword(dmai_src_H_reg) =00h;
55
   2
              Outword(dmai_src_L_reg) =00h;
23 2
              Outword(deal_cntrl_reg) =cloode; /* dest,sea,no inc/dec */
                                        /# source.I/O.inc toff-tc-int #/
                                     /# SYN-unused: on-P-TDRQ-CHG-ST-word #/
24 2
            END: /+ INITI86 PROC +/
         SETUP PROCEDURE OF THE 2681 DUART UTILITY
         25 1
             : B165 TIMI
           PROCEDURE PUBLIC:
```

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### PACHANE TEST BYTE :

### BECLAME TEST BYTE
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END INTI86;

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```
156 2
            END GETCH:
          PWM_SET_UP
          /+ this function is used to program the IXYS IXDP610 Digital Pulse Width
             Modulator to the fowing operating control byte
           SETUP PWM: PROCEDURE PUBLIC:
157 1
            DECLARE SET PORT ADDRESS;
158
   2
157 2
            DECLARE CONTROL LATCH literally '1302h';
            DECLARE (CONTROL BYTE, PWM_BYTE) WORD;
150 2
                                                /# BYTE:#/
                      PWM_CONTROL_BYTE
                      7-6-5-4-3-2-1-0
                              0-0-0 Dead time (0)
                            U----- Not Used
                           O----- Lock Bit (off)
                         O----- Divide Bit (no division)
                                    Resolution Bit (8-bit)
                      1----- Stop Bit (output enabled)
           SET PORT = 0:
161 2
5 561
           CONTROL BYTE = OCOH;
                                             /+ set the control byte
              SET_PORT = CONTROL_LATCH;
163
   2
                                              /# Set address of control port #/
              OUTPUT (SET PORT) = CONTROL BYTE;
                                              /# output coutrol byte
164
   5
165 2
              COUNT1 = 0:
                                              /* clear counter-0 to zero
166 2
              COUNTS = 1:
                             /# set counter-1 to 1 witch brings the cs in line #/
167 2
          END SETUP PWN:
          This procedure is interrupt driven by Timer 1 wich is used to count a #/
          7.8
                125khz 8m/s signal it is this timing that sets when the interrupt +/
          UPDATE PWM INT:
            PROCEDURE INTERRUPT 18 PUBLIC:
                                                 /* address of pwm latch
             DECLARE PW LATCH
                              literally '1300h';
169
            OECLARE EDI_REGISTER literally 'OFF22h'; /* End Of Interrupt resets IS*/
170
            DECLARE PWN DATA WORD:
171
   2
                                                 /# set bit 9 to one #/
172
            DECLARE HIGH WORD DATA (0200h);
                                           /# set bit 9 to zero #/
173
   2
            DECLARE LOW WORD DATA (0);
            DECLARE LEVEL WORD;
174
   3
             DECLARE PWN TABLE (+) WORD DATA
175
   2
               1000h.00Ah.014h.01Eh.028h.031h.038h.044h.048h.055h.
                05Eh.065h.06Ch.073h.079h.07Fh.084h.088h.08Ch.08Fh.
                092h,093h.094h.095h.094h.093h.092h.08Fh.08Ch.088h,
                394h.37fh.079h.073h.06Ch.065h.05Eh.055h.04Dh.044h.
                938h.631h.628h.01Eh.014h.00Ah.000h);
```